

Supplementary Materials for

Single-Crystal Elasticity of (Al,Fe)-bearing Bridgmanite up to 82 GPa

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Supplementary materials for single-crystal elasticity of (Al,Fe)-bearing bridgmanite consists of:

Texts S1-S3

Figures S1-S4

Tables S1-S3

Text S1. Data analyses on equation of state of single-crystal Fe10-Al14-Bgm. Collected high-pressure XRD patterns of single-crystal Fe10-Al14-Bgm were analyzed to determine its unit cell parameters and volumes (Figure S1 and Table S2). We fit the pressure-volume relationship at 300 K using a third-order Birch-Murnaghan equation of state (EoS) (Birch, 1978):

$$P = \frac{3}{2} K_{T0} \left[(V_0/V)^{\frac{7}{3}} - (V_0/V)^{\frac{5}{3}} \right] \left\{ 1 + \frac{3}{4} (K'_{T0} - 4) \left[(V_0/V)^{\frac{2}{3}} - 1 \right] \right\} \quad (1)$$

where K_{T0} (V_0) is the isothermal bulk modulus (unit cell volume) at ambient conditions, and K'_{T0} is the pressure derivative of K_{T0} . The best fits show $K_{T0} = 256 (\pm 2) \text{ GPa}$, $K'_{T0} = 4$ (fixed), or $K_{T0} = 259 (\pm 4) \text{ GPa}$, $K'_{T0} = 3.8 (\pm 0.2)$, with a fixed V_0 as 163.75 \AA^3 , consistent with early studies on (Al,Fe)-bearing bridgmanite within uncertainties (Boffa Ballaran et al., 2012; Mao et al., 2017).

Text S2. Fe partitioning between ferropericlase and bridgmanite as well as the spin crossover in ferropericlase. Early studies show that Fe partitioning coefficient between bridgmanite and ferropericlase (K_D , given by $[\text{Fe}^{2+} + \text{Fe}^{3+}]_{\text{Bgm}} / [\text{Mg}^{2+}]_{\text{Bgm}} / ([\text{Fe}^{2+}]_{\text{Fp}} / [\text{Mg}^{2+}]_{\text{Fp}})$) could vary significantly with depth as a result of the spin crossover in ferropericlase (Irifune et al., 2010). Using literature K_D in a pyrolitic system (Irifune et al., 2010) for our modeling, Fe content in ferropericlase would change with depth in the lower mantle. Here we assume a linear Fe effect on K_S , μ and ρ of high-spin (HS) and low-spin (LS) ferropericlase and fit the literature data together (Figure S2) (Fei et al., 2007; Mao et al., 2011; Marquardt et al., 2009; Speziale et al., 2001; Yang et al., 2016; Yang et al., 2015). The best fits to density using Birch-Murnaghan EoS with fixed $K'_{T0} = 4$ show:

$$\rho_{0_HS}(\text{Fe}) = 3.58 + 2.40 \text{Fe}_{\text{Fp}}; K_{T0_HS}(\text{Fe}) = 159.5 - 11.8 \text{Fe}_{\text{Fp}} \quad (2)$$

$$\rho_{0_LS}(\text{Fe}) = 3.58 + 2.83 \text{Fe}_{\text{Fp}}; K_{T0_LS}(\text{Fe}) = 153.3 + 40.5 \text{Fe}_{\text{Fp}} \quad (3)$$

where Fe_{Fp} is the Fe content in ferropericlase, given as $\text{Fe}_{\text{Fp}} = \text{Fe} / (\text{Fe} + \text{Mg})$, and subscripts “HS” and “LS” indicate properties of HS and LS ferropericlase, respectively, with the same denotation for other

parameters in the followings. Analyses of literature reports (Wu et al., 2013; Yang et al., 2015) were used for Fe effect on μ of ferropericlasel:

$$\mu_{0_HS}(Fe) = 129 - 81.8Fe_{Fp}; \mu'_{0_HS}(Fe) = 2.32 - 1.97Fe_{Fp} \quad (4)$$

$$\mu_{0_LS}(Fe) = 142 - 81.8Fe_{Fp}; \mu'_{0_LS}(Fe) = 2.23 - 1.97Fe_{Fp} \quad (5)$$

To evaluate the spin crossover effect on K_S , μ , and ρ of ferropericlasel, we followed the literature modeling procedure (Mao et al., 2011; Wu et al., 2013; Yang et al., 2015) using:

$$V(n) = nV_{LS} + (1 - n)V_{HS} \quad (6)$$

$$\frac{V(n)}{K_S(n)} = n \frac{V_{LS}}{K_{S_{LS}}} + (1 - n) \frac{V_{HS}}{K_{S_{HS}}} - (V_{LS} - V_{HS}) \frac{\partial n}{\partial P} \bigg|_T \quad (7)$$

$$\frac{V(n)}{\mu(n)} \approx n \frac{V_{LS}}{\mu_{LS}} + (1 - n) \frac{V_{HS}}{\mu_{HS}} \quad (8)$$

where n is the LS fraction at high P-T. We note that studies indicate that the Fe effect on the onset pressure and width of the spin crossover is negligible for relatively Fe-poor ferropericlasel (<25 mol% Fe), but becomes complex for the Fe-rich (Mg,Fe)O counterpart (Speziale et al., 2007). Our modeling is limited to ferropericlasel containing less than 25 mol% Fe, which is most relevant to the lower-mantle composition.

Text S3. Thermoelastic modeling of ferropericlasel and davemaoite at high P-T. High P-T elastic data on different compositional ferropericlasel (e.g., Fan et al., 2019; Mao et al., 2011; Yang et al., 2016) are used to evaluate the effects of Fe as well as the spin crossover on its elastic properties (Figure S2 and Table S3) (Fan et al., 2019; Marquardt et al., 2009; Yang et al., 2015). Our modeled high P-T velocity profiles are compared with *ab initio* calculations on $Mg_{0.8126}Fe_{0.1875}O$ ferropericlasel (Wu et al., 2013) to evaluate the reliability of the constrained θ_0 , γ_0 , and q_0 values and their corresponding uncertainties (Stixrude and Lithgow-Bertelloni, 2005; Wentzcovitch et al., 2004; Wolf et al., 2015). We also

determined the thermoelastic parameters of CaSiO_3 davemaoite by refitting and benchmarking high P-T elastic data from experiments (Gréaux et al., 2019; Sun et al., 2016) and theoretical calculations (Kawai and Tsuchiya, 2015; Li et al., 2006) (Figure S3 and Table S3). Our modeled results fall into the range of theoretical calculations (Kawai and Tsuchiya, 2015; Li et al., 2006). We note that the data of davemaoite by Thomson et al. (2019) were not used here because they reported a much lower density profile than those by Gréaux et al. (2019) and Sun et al. (2016).

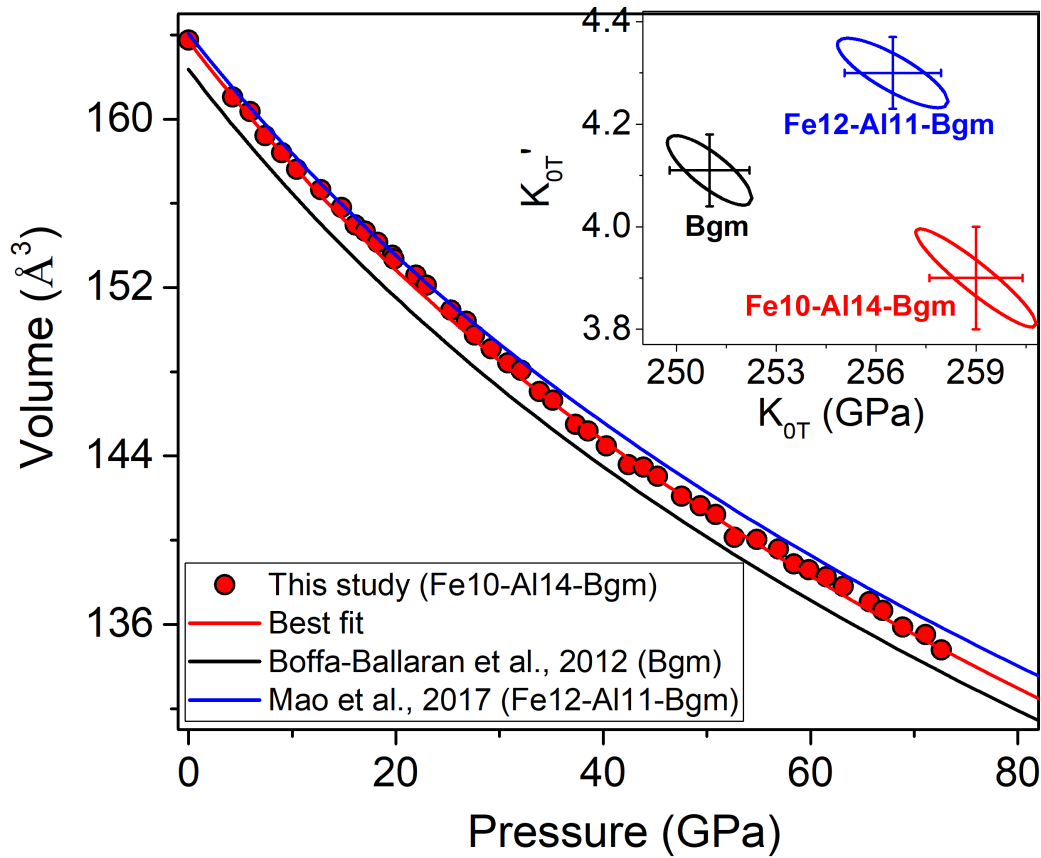


Figure S1. Unit-cell volumes of single-crystal Fe10-Al14-Bgm at high pressure and 300 K. Solid red circles are collected data of Fe10-Al14-Bgm in this study and the red line is the best fit using third-order Birch-Murnaghan EoS. Black and blue lines are literature results on MgSiO₃ bridgmanite end member (Boffa Ballaran et al., 2012) and (Al,Fe)-bearing bridgmanite with Mg_{0.89}Fe²⁺_{0.024}Fe³⁺_{0.096}Al_{0.11}Si_{0.89}O₃ composition (Fe12-Al11-Bgm) (Mao et al., 2017), respectively. The insert shows derived error ellipses of K_{OT} and K'_{OT} at the $\pm 1\sigma$ level.

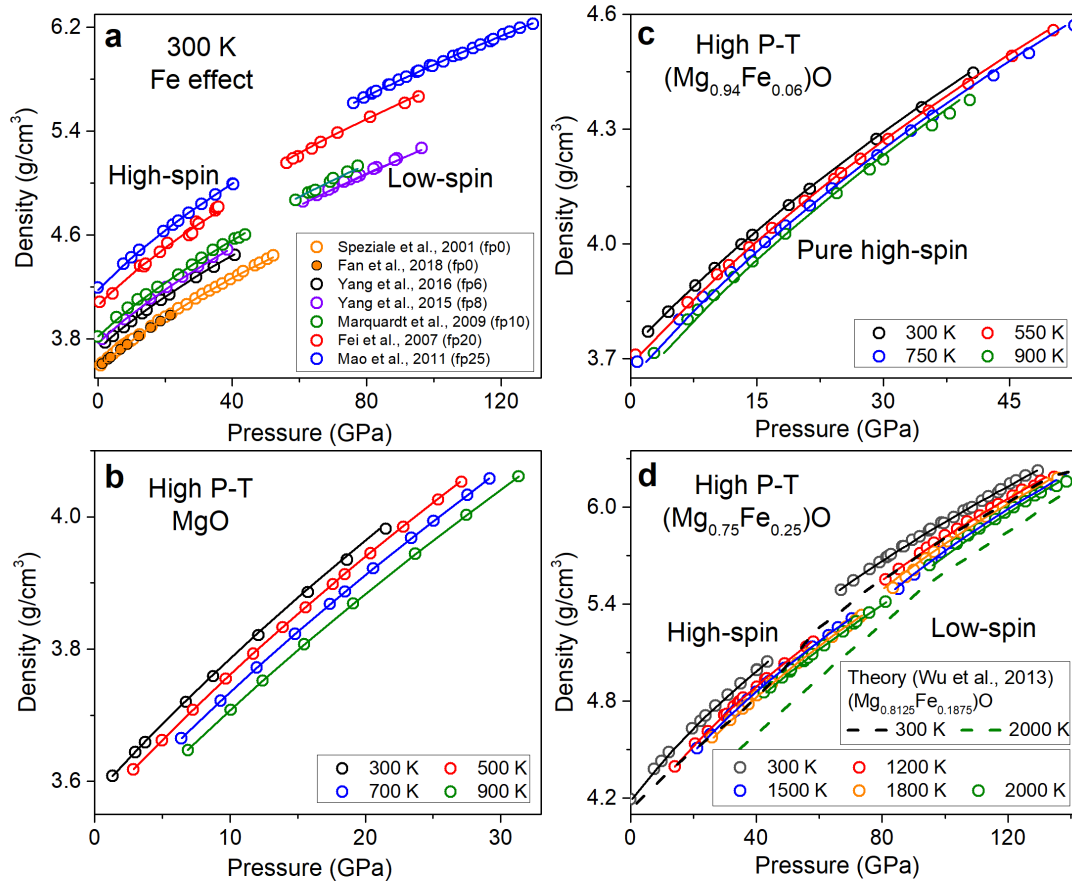


Figure S2. Modeling on thermoelastic properties of ferropericlase at high P-T. **a** is density of ferropericlase with different Fe contents at high pressure and 300 K, while **b-d** are high P-T data from the literature. In **a**, symbols are experimental data (Fei et al., 2007; Mao et al., 2011; Marquardt et al., 2009; Speziale et al., 2001; Yang et al., 2016; Yang et al., 2015), and solid lines with corresponding colors are the best fits using Birch-Murnaghan EoS. A linear Fe effect on the density of ferropericlase is assumed. Detailed references are shown in the legend, in which numbers in parentheses right after “fp” indicate its Fe content in molar per cent. In **b-d**, symbols are high P-T elastic data of MgO (Fan et al., 2019), (Mg_{0.94}Fe_{0.06})O (Yang et al., 2016), and (Mg_{0.75}Fe_{0.25})O (Mao et al., 2011), and solid lines are the best fits using the self-consistent thermoelastic model. Theoretical calculations on (Mg_{0.8125}Fe_{0.1875})O ferropericlase (Wu et al., 2013) are plotted as dashed black (300 K) and olive (2000 K) in **d** for comparisons. Uncertainties are smaller than symbols when not shown.

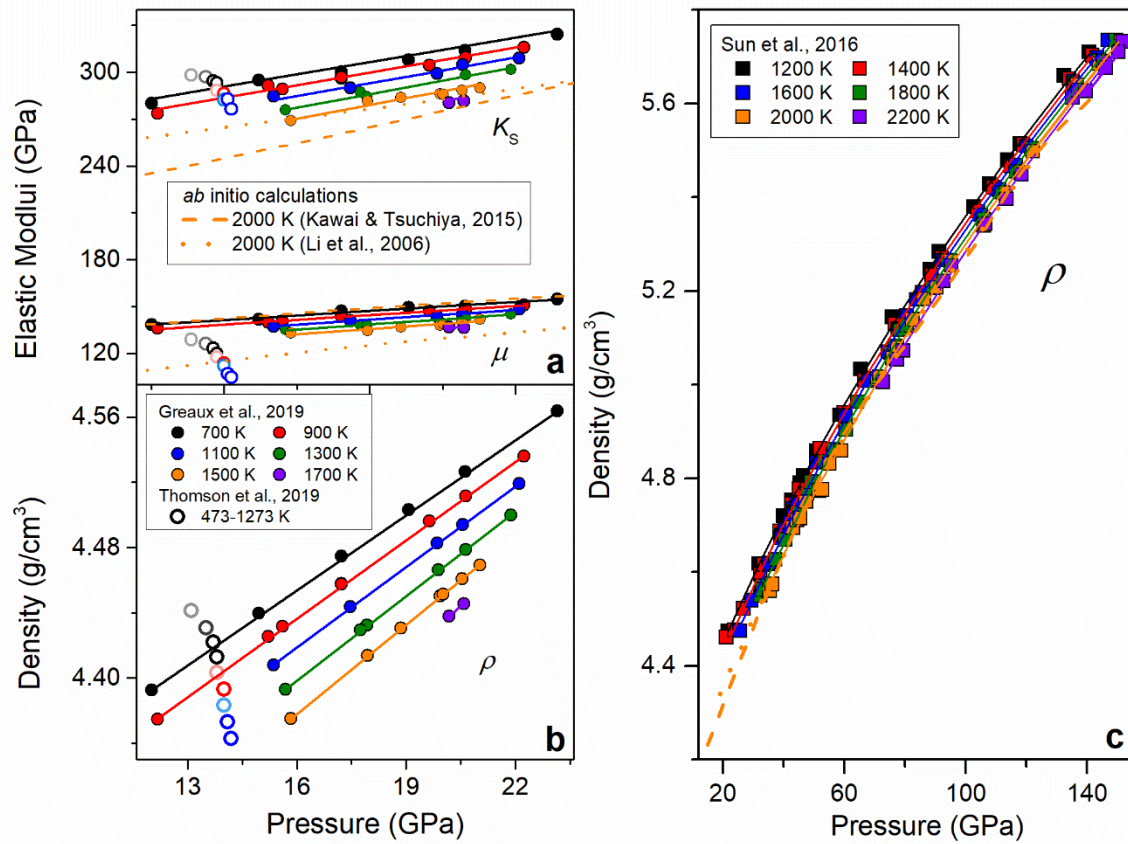


Figure S3. Modeling on thermoelastic parameters of CaSiO_3 davemaoite at high P-T. **a** and **b-c** show high P-T elastic moduli (K_s and μ) and density of davemaoite, respectively. In **a** and **b**, solid symbols are data from Gréaux et al. (2019), and solid lines are the best fits. Open circles are data from Thomson et al. (2019), which show much lower shear moduli than those from Gréaux et al. (2019) and are not included in our fitting. **c** is thermal EoS of CaSiO_3 davemaoite (Sun et al., 2016) up to 150 GPa and 2200 K, which is consistent with those by Gréaux et al. (2019) and is included in our constraints. Dashed (Kawai and Tsuchiya, 2015) and dotted (Li et al., 2006) lines are from theoretical calculations at 2000 K. Uncertainties are smaller than symbols when not shown.

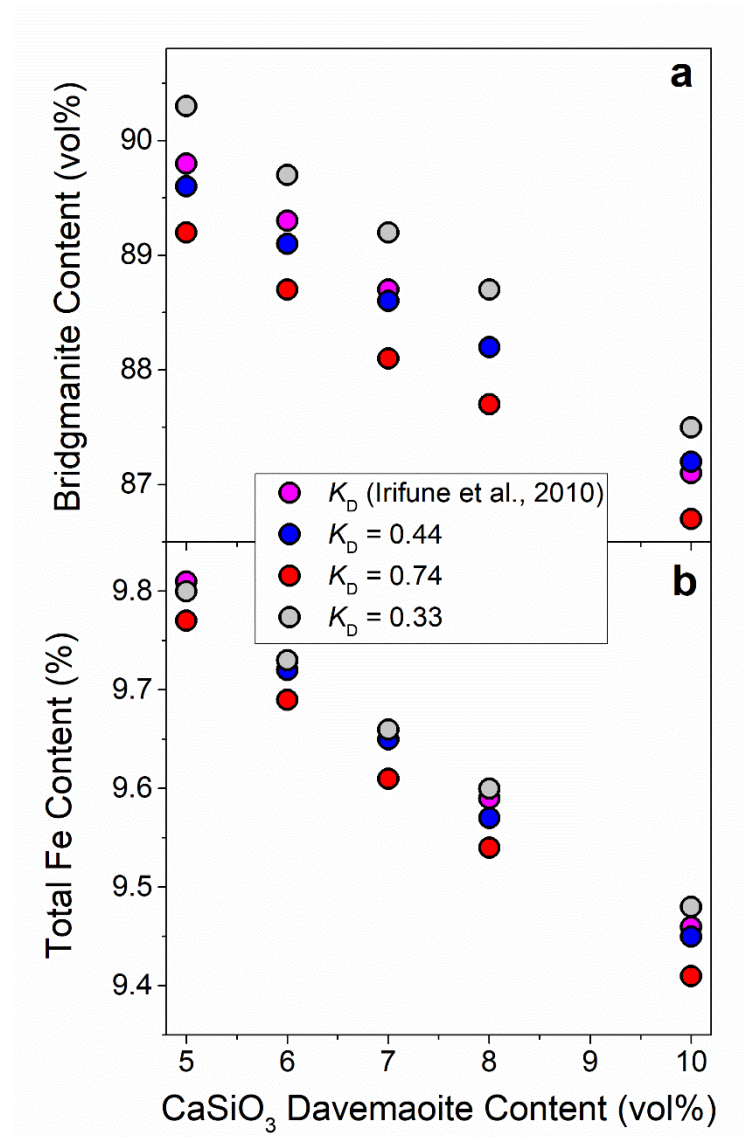


Figure S4. Trade-offs between volume and compositional parameters on deriving the lower-mantle composition. **a**, Volume percentages of bridgmanite versus CaSiO₃ davemaoite. **b**, Total Fe content versus the volume percentage of CaSiO₃ davemaoite. Pink circles are our best-fit model with K_D varying with depth (Irifune et al., 2010). Blue, red, and gray circles are results with fixed K_D as 0.44, 0.74, and 0.33, respectively. These K_D values are chosen to cover its range in literature reports (Irifune et al., 2010).

| | | | | | | |
|-----|----------|----------|----------|---|----------|----------|
| 0 | 12.20(6) | 6.984(7) | 7.150(6) | - | 6.970(8) | - |
| 10 | 12.04(6) | 6.921(8) | 7.237(6) | - | 6.941(8) | - |
| 20 | 11.90(6) | 6.873(8) | 7.328(6) | - | 6.952(7) | - |
| 30 | 11.73(7) | 6.848(8) | 7.367(6) | - | 6.971(7) | - |
| 40 | 11.82(7) | 6.812(8) | 7.457(7) | - | 6.996(7) | - |
| 50 | - | 6.788(7) | 7.363(7) | - | 6.990(7) | - |
| 60 | 12.04(7) | 6.891(7) | 7.373(8) | - | 6.920(7) | 7.190(7) |
| 70 | - | 6.947(7) | 7.249(8) | - | 6.850(6) | 7.230(8) |
| 80 | - | 7.013(7) | - | - | 6.870(6) | 7.270(8) |
| 90 | - | 7.036(7) | - | - | 6.880(6) | 7.220(7) |
| 100 | - | 7.088(6) | - | - | 6.890(6) | 6.930(7) |
| 110 | 12.37(6) | 7.105(6) | - | - | 6.936(7) | - |
| 120 | 12.43(6) | 7.134(6) | - | - | 6.887(7) | - |
| 130 | 12.37(6) | 7.142(6) | - | - | 7.020(7) | - |
| 140 | 12.37(7) | 7.144(6) | - | - | 7.090(7) | - |
| 150 | - | 7.145(6) | - | - | 7.030(7) | 7.220(8) |
| 160 | - | 7.135(6) | - | - | 6.992(8) | - |
| 170 | 12.20(7) | 7.090(7) | - | - | 7.026(8) | - |
| 180 | 12.10(7) | 6.869(7) | 7.249(7) | - | 7.026(8) | - |
| 190 | - | 6.855(6) | 7.340(8) | - | 6.961(6) | - |
| 200 | 11.90(7) | 6.833(6) | 7.370(8) | - | 6.944(8) | - |

54.4 (6) GPa

| | | | | | | |
|-----|----------|----------|----------|---|----------|----------|
| 0 | 12.38(7) | 7.028(8) | 7.311(7) | - | 7.011(7) | - |
| 10 | 12.21(7) | 6.981(8) | 7.380(7) | - | 7.051(6) | - |
| 20 | 12.10(8) | 6.942(7) | 7.456(7) | - | 7.059(6) | - |
| 30 | 11.92(8) | 6.908(7) | 7.520(8) | - | 7.081(6) | - |
| 40 | - | 6.895(7) | 7.501(8) | - | 7.090(6) | - |
| 50 | 12.02(7) | 6.924(7) | 7.509(8) | - | 7.086(8) | - |
| 60 | - | 6.862(8) | 7.393(6) | - | 6.950(8) | 7.140(7) |
| 70 | - | 6.940(9) | 7.341(6) | - | 6.920(8) | 7.230(7) |
| 80 | 12.36(7) | 7.000(9) | 7.463(6) | - | 6.970(8) | 7.310(9) |
| 90 | 12.46(8) | 7.079(8) | - | - | 6.930(8) | 7.350(9) |
| 100 | - | 7.102(8) | - | - | 6.920(8) | - |
| 110 | 12.62(7) | 7.197(8) | - | - | 7.059(8) | - |
| 120 | 12.66(8) | 7.274(8) | - | - | 6.920(8) | - |
| 130 | 12.62(8) | 7.235(8) | - | - | 7.081(8) | - |
| 140 | - | 7.237(8) | - | - | 7.090(7) | - |
| 150 | 12.52(9) | 7.219(7) | - | - | 7.039(7) | - |
| 160 | - | 7.147(7) | - | - | 7.050(7) | - |
| 170 | - | 7.026(6) | - | - | 7.020(7) | - |
| 180 | 12.36(7) | 6.944(6) | 7.381(7) | - | 7.048(7) | - |
| 190 | 12.21(8) | 6.937(6) | 7.479(6) | - | 7.093(7) | - |
| 200 | 12.10(8) | 6.943(7) | 7.543(8) | - | 7.050(6) | - |

65.8 (8) GPa

| | | | | | | |
|----|----------|----------|----------|---|----------|----------|
| 0 | 12.50(8) | 7.039(7) | 7.589(9) | - | 7.076(7) | - |
| 10 | 12.33(8) | 7.086(7) | 7.590(9) | - | 7.030(7) | 7.420(9) |
| 20 | 12.20(8) | 7.125(8) | 7.683(9) | - | - | 7.236(9) |
| 30 | - | 7.122(8) | 7.646(8) | - | 7.070(7) | 7.269(9) |
| 40 | 12.10(8) | 7.112(8) | 7.709(8) | - | - | 7.210(7) |
| 50 | - | 7.104(8) | 7.633(7) | - | 7.122(8) | - |

| | | | | | | |
|--------------|-----------|-----------|-----------|---|-----------|-----------|
| 60 | 12.30(7) | 7.042(8) | 7.542(7) | - | 7.086(8) | - |
| 70 | 12.50(7) | 6.997(8) | 7.525(7) | - | 7.135(8) | - |
| 80 | 12.64(7) | 7.036(9) | 7.514(8) | - | 7.147(8) | - |
| 90 | - | 7.069(9) | - | - | 7.189(8) | - |
| 100 | 12.80(9) | 7.212(9) | - | - | 7.260(8) | - |
| 110 | - | 7.316(7) | - | - | 7.180(9) | 7.430(8) |
| 120 | 12.80(9) | 7.394(8) | - | - | 7.120(9) | - |
| 130 | 12.80(9) | 7.410(7) | - | - | 7.160(7) | 7.510(8) |
| 140 | - | 7.359(9) | - | - | 7.193(7) | - |
| 150 | 12.70(9) | 7.298(9) | - | - | 7.136(7) | - |
| 160 | - | 7.137(8) | - | - | 7.140(7) | - |
| 170 | - | 7.105(8) | 7.50(8) | - | 7.075(8) | - |
| 180 | 12.53(7) | 7.054(8) | 7.57(8) | - | 7.113(8) | - |
| 190 | 12.34(7) | 7.048(7) | 7.57(9) | - | 7.050(8) | - |
| 200 | - | 7.103(7) | 7.55(9) | - | 7.256(8) | - |
| <hr/> | | | | | | |
| 70.4 (7) GPa | | | | | | |
| 0 | 12.53(9) | 7.078(9) | 7.603(8) | - | 7.160(9) | - |
| 10 | 12.40(9) | 7.106(8) | 7.647(9) | - | 7.090(9) | - |
| 20 | - | 7.175(8) | 7.730(9) | - | - | 7.333(9) |
| 30 | 12.14(9) | 7.161(8) | 7.690(9) | - | - | 7.280(9) |
| 40 | - | 7.171(8) | 7.680(9) | - | - | 7.279(10) |
| 50 | 12.30(8) | 7.137(8) | 7.671(8) | - | 7.185(9) | - |
| 60 | 12.36(8) | 7.097(9) | 7.639(8) | - | 7.140(9) | - |
| 70 | - | 7.063(9) | 7.612(8) | - | 7.121(9) | - |
| 80 | - | 7.052(9) | 7.541(8) | - | 7.145(9) | - |
| 90 | 12.80(8) | 7.097(9) | 7.497(9) | - | 7.227(9) | - |
| 100 | - | 7.293(9) | - | - | 7.190(8) | 7.540(10) |
| 110 | 12.90(8) | 7.394(9) | - | - | 7.190(8) | 7.510(9) |
| 120 | - | 7.466(9) | - | - | 7.180(8) | - |
| 130 | 12.90(9) | 7.490(9) | - | - | 7.283(8) | 7.512(8) |
| 140 | 12.86(9) | 7.416(8) | - | - | 7.243(8) | - |
| 150 | - | 7.214(8) | 7.439(9) | - | 7.171(8) | - |
| 160 | 12.75(9) | 7.144(9) | 7.588(9) | - | 7.160(9) | - |
| 170 | - | 7.119(9) | - | - | 7.115(9) | - |
| 180 | 12.60(7) | 7.084(10) | 7.639(9) | - | 7.188(9) | - |
| 190 | 12.45(9) | 7.134(8) | 7.661(10) | - | - | 7.380(9) |
| 200 | - | 7.169(7) | 7.692(9) | - | - | 7.290(9) |
| <hr/> | | | | | | |
| 76.0 (9) GPa | | | | | | |
| 0 | - | 7.096(8) | 7.654(10) | - | 7.110(8) | 7.530(10) |
| 10 | 12.44(9) | 7.155(9) | 7.700(10) | - | - | 7.410(10) |
| 20 | 12.33(9) | 7.252(9) | 7.766(10) | - | - | 7.390(10) |
| 30 | 12.20(9) | 7.220(10) | 7.733(10) | - | - | 7.320(10) |
| 40 | 12.30(10) | 7.239(10) | 7.743(10) | - | - | 7.220(9) |
| 50 | 12.36(11) | 7.224(10) | 7.757(9) | - | 7.238(9) | - |
| 60 | - | 7.149(10) | 7.689(9) | - | 7.167(9) | - |
| 70 | - | 7.105(9) | 7.621(9) | - | 7.163(9) | - |
| 80 | 12.75(9) | 7.073(9) | 7.585(9) | - | 7.216(9) | - |
| 90 | - | 7.107(9) | 7.541(9) | - | 7.278(9) | - |
| 100 | 12.92(9) | 7.345(9) | - | - | 7.300(10) | 7.550(9) |
| 110 | - | 7.469(9) | - | - | - | 7.553(9) |

| | | | | | | |
|---------------|-----------|-----------|-----------|---|-----------|-----------|
| 120 | 12.92(9) | 7.543(9) | - | - | - | 7.544(9) |
| 130 | - | 7.553(9) | - | - | 7.381(10) | 7.510(9) |
| 140 | 12.90(8) | 7.487(9) | - | - | 7.318(9) | - |
| 150 | - | 7.377(9) | - | - | 7.239(9) | - |
| 160 | 12.80(8) | 7.185(9) | 7.655(10) | - | 7.135(9) | - |
| 170 | - | 7.170(10) | 7.683(10) | - | 7.137(9) | - |
| 180 | - | 7.135(10) | 7.733(10) | - | 7.160(9) | - |
| 190 | 12.47(9) | 7.174(10) | 7.757(11) | - | - | 7.410(9) |
| 200 | 12.33(9) | 7.206(10) | 7.747(10) | - | - | 7.390(9) |
| 82.0 (14) GPa | | | | | | |
| 0 | - | 7.113(10) | 7.705(11) | - | 7.302(9) | - |
| 10 | 12.54(10) | 7.205(10) | 7.752(11) | - | - | 7.531(11) |
| 20 | 12.38(10) | 7.329(10) | 7.803(11) | - | - | 7.570(11) |
| 30 | 12.27(10) | 7.325(12) | 7.776(11) | - | - | 7.680(11) |
| 40 | 12.38(10) | 7.306(12) | 7.806(12) | - | 7.196(9) | 7.614(12) |
| 50 | 12.49(11) | 7.311(11) | 7.843(12) | - | 7.103(10) | 7.560(12) |
| 60 | - | 7.202(11) | 7.740(12) | - | 7.080(10) | - |
| 70 | 12.71(11) | 7.147(11) | 7.630(12) | - | 7.050(10) | - |
| 80 | - | 7.094(12) | 7.628(10) | - | - | 7.275(11) |
| 90 | - | 7.111(12) | 7.710(10) | - | - | 7.300(13) |
| 100 | 12.94(12) | 7.478(12) | - | - | 7.433(11) | 7.550(13) |
| 110 | - | 7.617(11) | - | - | 7.605(11) | - |
| 120 | 13.00(12) | 7.701(11) | - | - | 7.400(11) | - |
| 130 | 13.00(12) | 7.705(12) | - | - | 7.435(10) | 7.510(11) |
| 140 | - | 7.646(9) | - | - | 7.391(9) | - |
| 150 | 12.94(9) | 7.313(9) | - | - | 7.322(9) | - |
| 160 | - | 7.236(9) | 7.730(10) | - | 7.265(9) | - |
| 170 | 12.82(11) | 7.171(9) | 7.776(10) | - | 7.298(11) | - |
| 180 | - | 7.186(9) | 7.716(10) | - | 7.246(10) | - |
| 190 | - | 7.253(10) | 7.800(12) | - | - | 7.601(10) |
| 200 | - | 7.330(9) | 7.840(11) | - | - | 7.610(10) |

Table S2. Unit-cell parameters of single-crystal Fe10-Al14-Bgm at high pressure

| Au | | Fe10-Al14-Bgm | | | |
|-------------------|--------------|---------------|--------------|--------------|----------------------------|
| Pressure (GPa) | <i>a</i> (Å) | <i>a</i> (Å) | <i>b</i> (Å) | <i>c</i> (Å) | <i>V</i> (Å ³) |
| ambient | | 4.7875(2) | 4.9423(2) | 6.9205(2) | 163.75(1) |
| 4.3(1) | 4.0463(3) | 4.7601(2) | 4.9122(2) | 6.8873(2) | 161.04(1) |
| 5.9(1) | 4.0348(3) | 4.7526(2) | 4.9056(2) | 6.8776(2) | 160.35(1) |
| 7.4(1) | 4.0253(3) | 4.7375(2) | 4.9029(2) | 6.8544(2) | 159.21(1) |
| 9.0(1) | 4.0151(3) | 4.7282(2) | 4.8971(2) | 6.8410(2) | 158.40(2) |
| 10.4(1) | 4.0064(3) | 4.7244(2) | 4.8868(2) | 6.8269(3) | 157.62(2) |
| 12.8(1) | 3.9930(3) | 4.7131(2) | 4.8805(2) | 6.8099(3) | 156.64(2) |
| 14.8(1) | 3.9820(3) | 4.7023(3) | 4.8745(2) | 6.7969(3) | 155.79(2) |
| 16.1(1) | 3.9750(3) | 4.6967(3) | 4.8638(2) | 6.7845(3) | 154.98(2) |
| 17.1(1) | 3.9701(3) | 4.6952(3) | 4.8599(2) | 6.7782(3) | 154.67(2) |
| 18.3(1) | 3.9640(3) | 4.6897(3) | 4.8538(2) | 6.7720(3) | 154.15(2) |
| 19.6(1) | 3.9573(3) | 4.6821(3) | 4.8483(2) | 6.7640(3) | 153.54(3) |
| 19.8(1) | 3.9564(3) | 4.6812(3) | 4.8455(2) | 6.7605(3) | 153.35(3) |
| 21.9(1) | 3.9464(3) | 4.6744(3) | 4.8403(3) | 6.7436(3) | 152.58(3) |
| 22.9(1) | 3.9418(3) | 4.6678(3) | 4.8357(3) | 6.7390(3) | 152.11(3) |
| 25.3(1) | 3.9313(3) | 4.6623(3) | 4.8143(3) | 6.7239(3) | 150.92(3) |
| 26.8(1) | 3.9249(3) | 4.6562(3) | 4.8113(3) | 6.7136(4) | 150.40(4) |
| 27.6(2) | 3.9217(4) | 4.6485(3) | 4.8034(3) | 6.7061(4) | 149.74(4) |
| 29.2(2) | 3.9150(4) | 4.6406(3) | 4.7962(3) | 6.6985(4) | 149.09(4) |
| 30.8(2) | 3.9086(4) | 4.6316(3) | 4.7906(3) | 6.6894(4) | 148.42(4) |
| 32.1(2) | 3.9036(5) | 4.6364(3) | 4.7873(3) | 6.6709(4) | 148.06(4) |
| 33.8(2) | 3.8969(6) | 4.6143(3) | 4.7812(3) | 6.6660(4) | 147.06(5) |
| 35.1(2) | 3.8920(6) | 4.6204(4) | 4.7689(3) | 6.6555(4) | 146.65(5) |
| 37.3(2) | 3.8840(6) | 4.5977(4) | 4.7574(3) | 6.6488(5) | 145.50(5) |
| 38.6(3) | 3.8797(7) | 4.5989(4) | 4.7566(3) | 6.6374(5) | 145.19(5) |
| 40.3(3) | 3.8736(8) | 4.5913(4) | 4.7502(3) | 6.6246(5) | 144.48(5) |
| 42.4(3) | 3.8664(9) | 4.5813(4) | 4.7412(3) | 6.6110(5) | 143.59(5) |
| 43.9(3) | 3.8617(9) | 4.5848(4) | 4.7477(3) | 6.5905(5) | 143.46(6) |
| 45.2(4) | 3.8573(10) | 4.5800(4) | 4.7424(4) | 6.5850(5) | 143.03(6) |
| 47.6(4) | 3.8498(10) | 4.5676(4) | 4.7356(4) | 6.5691(5) | 142.09(6) |
| 49.4(4) | 3.8443(10) | 4.5645(4) | 4.7286(4) | 6.5622(5) | 141.64(6) |
| 50.8(4) | 3.8398(11) | 4.5562(5) | 4.7266(4) | 6.5574(5) | 141.22(6) |
| 52.7(4) | 3.8344(10) | 4.5494(5) | 4.7102(4) | 6.5396(6) | 140.13(6) |
| 54.8(4) | 3.8281(11) | 4.5464(5) | 4.7109(4) | 6.5382(6) | 140.03(6) |
| 56.9(5) | 3.8222(11) | 4.5358(5) | 4.7042(4) | 6.5410(6) | 139.57(6) |
| 58.4(5) | 3.8181(11) | 4.5236(5) | 4.7000(4) | 6.5314(6) | 138.86(7) |
| 59.9(5) | 3.8141(11) | 4.5225(6) | 4.6956(4) | 6.5266(6) | 138.60(7) |
| 61.5(5) | 3.8097(11) | 4.5172(6) | 4.6938(5) | 6.5205(6) | 138.26(7) |
| 63.1(5) | 3.8053(11) | 4.5080(6) | 4.6910(5) | 6.5163(6) | 137.80(7) |
| 65.7(4) | 3.7987(10) | 4.4973(6) | 4.6823(5) | 6.5091(6) | 137.07(7) |
| 67.0(5) | 3.7954(10) | 4.4877(6) | 4.6814(5) | 6.5046(6) | 136.66(7) |
| 68.9(5) | 3.7907(10) | 4.4701(6) | 4.6766(5) | 6.4994(7) | 135.87(7) |
| 71.1(5) | 3.7853(11) | 4.4719(6) | 4.6700(5) | 6.4887(7) | 135.51(7) |
| 72.6(5) | 3.7816(11) | 4.4567(6) | 4.6661(5) | 6.4810(7) | 134.78(7) |

Table S3. Thermoelastic parameters of lower-mantle major minerals for high P-T modeling

| | V_0 (Å ³) | K_0 (GPa) | K'_0 | μ_0 (GPa) | μ'_0 | θ_0 | γ_0 | q_0 | η_{s0} |
|---|-------------------------|----------------|--------|------------------|----------|------------|------------|-------|-------------|
| ^a (Al,Fe)-bearing Bridgmanite | - | - | - | - | - | 900 | 1.57 | 1.1 | 2.4 |
| ^a Ferropericlase (HS) | - | - | - | - | - | 760 | 1.4 | 1.2 | 2.6 |
| ^a Ferropericlase (LS) | - | - | - | - | - | 760 | 1.4 | 0.3 | 2.6 |
| ^b CaSiO ₃ davemaoite | 45.4 | 248 | 4 | 126 | 1.6 | 1000 | 1.42 | 2.65 | 1.54 |

^aSee details in main text and supplementary text S2 for Fe and/or Al effects on V_0 , K_0 , K'_0 , μ_0 , and μ'_0 of (Al,Fe)-bearing bridgmanite and ferropericlase. Values of θ_0 , q_0 , γ_0 , and η_{s0} for (Al,Fe)-bearing bridgmanite and ferropericlase are constrained by benchmarking from literature experimental data together with *ab initio* calculations (Fiquet et al., 2000; Mao et al., 2011; Shim and Duffy, 2000; Stixrude and Lithgow-Bertelloni, 2005; Tange et al., 2012; Wentzcovitch et al., 2004; Wolf et al., 2015).

^bThermoelastic parameters for CaSiO₃ davemaoite are derived by refitting literature data (Gréaux et al., 2019; Sun et al., 2016) with the model.

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